

substituting the relation (8a) into (16), we have

$$R_y^{1/2} = (I + A^{-1}\Psi K_g)R_\epsilon^{1/2}. \tag{17}$$

The matrix Ψ acts as a shift operator on the block columns of K_g , so that ΨK_g is a lower block banded matrix, cf. (8b). Denote

$$K = \Psi K_g \tag{18}$$

then K is lower block banded and

$$R_y^{1/2} = (I + A^{-1}K)R_\epsilon^{1/2}. \tag{19}$$

The Mapping Result

Comparing now the two results (12) and (19) for the covariance factor $R_y^{1/2}$, we find

$$(I + A^{-1}K)R_\epsilon^{1/2} = A^{-1}\tilde{C}. \tag{20}$$

Let

$$C = \tilde{C}R_\epsilon^{-1/2} \tag{21}$$

then we conclude

$$K = C - A. \tag{22}$$

The global relation (22) can be reduced to a local one by noting that the matrices K , C , and A are all lower block banded, hence

$$K_i = C_i - A_i \tag{23}$$

where K_i (respectively, C_i , A_i) is the i th block column of K (respectively, C , A). Now notice from (18) that K_i corresponds to the Kalman gain $K_{g_{i+1,i}}$, so that we have obtained an alternative expression for the Kalman gains at different times in terms of Wiener theory. This result generalizes the stationary one in [8, p. 662], [9, p. 173], and [10, ch. 7].

We should note that the factorization of a block matrix is not unique, and that (22) is true under the *block* factorization (11), giving the block banded C necessary for a recursive realization of (12). Also notice that the mapping result (23) does not show yet how one can get the matrix $R_\epsilon^{1/2}$ from the multivariable Wiener theory. However, by noting from (14c) and (18) that K has to be strictly lower banded, it is clear that $R_\epsilon^{1/2} = C_i^{-1} = \tilde{C}_i$.

IV. CONCLUSION

A relationship between Wiener theory and Kalman filtering has been presented for nonstationary finite-dimensional processes. The results give an expression for the Kalman gain in terms of the innovation filter by Wiener theory, which generalizes the stationary case. Similar relations can be found for the filter and smoothing estimators.

The main difference between the modes of this paper and others which used matrix operators to model time varying processes, e.g., in [4]-[6] and [13], [14], is our use of system operators in MFD forms along with their connection to state-space forms. Several additional general results for time-varying realizations of multivariable linear systems are given in [7]. Here we note that among other possible realizations of the system operator matrix, the one by diagonals turns out to be intimately related to the ladder form. The advantages of this form, including modular structure and good numerical behavior makes it even more attractive for future research.

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A Simulation Aid to Gain Estimates for Robust Tuning Regulators

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Abstract—Gain estimates for Davison's robust tuning regulator are shown to be directly computable from plant open-loop step data using low-order simulation techniques. At no stage of the procedure is a detailed model of plant dynamics required.

I. INTRODUCTION

The robust tuning regulator originally proposed by Davison [1] provides a simple but effective way of generating integrating process controllers without the need to have a detailed model of the plant available. More precisely, given the m -input/ m -output *stable* multivariable plant described by the state-space model

$$\begin{aligned} \dot{x}(t) &= Ax(t) + Bu(t) \\ y(t) &= Cx(t) \end{aligned} \tag{1}$$

in R^n , the integrating unity negative output feedback controller with transfer function matrix

$$K(s) = G^{-1}(o) \frac{\epsilon}{s} \tag{2}$$

will stabilize the plant, reject constant disturbances, and track step set-point changes for gains ϵ in some (nonempty) range $0 < \epsilon < \epsilon^*$ provided that $G(o)$ is nonsingular. The matrix $G(o)$ can be computed directly from the plant transfer function matrix $G(s) = C(sI - A)^{-1}B$ (if available) or

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